

instructions (e.g., receive instructions to perform a self-test, receive instructions to “trip” (interrupt the circuit), receive instructions to “reset”, etc.).

**[0056]** It should be understood by a person of ordinary skill in the art that the individual blocks represented in FIG. 1A do not necessarily represent individual components. Rather any suitable combination of these blocks may be implemented by a single component such as, but not limited to, a microprocessor, integrated circuit, or the like. Similarly, any given block may be implemented by more than one circuit component without departing from the spirit of the invention.

**[0057]** As shown in FIGS. 6 and 7, the AFCI system 5 can be sized and arranged to be disposed within a housing 200, the housing being configured to be installed in a single gang electrical enclosure, e.g., a wall-box mounted AFCI. In other embodiments, the AFCI system may be housed or mounted in any suitable form factor such as, but not limited to, a circuit breaker, a panel mount device, an in-line device, or the like.

**[0058]** Alternative embodiments of an AFCI system 6, 6.1 and 6.2 are shown in FIGS. 3A, 3B, and 3C. FIGS. 3D, 3E, and 3F are more detailed views of the components in the embodiment in FIG. 3C. Any of these embodiments of the AFCI system may employ any one of the wiring configurations shown in FIGS. 1B-1F, or any one of the sensor configurations shown in FIGS. 2C-2F.

**[0059]** As illustrated in FIG. 1A, device 5 includes line side connections 11 and load side connections 70. Line side connections 11 include a first line contact 12 and a second line contact 14. First line contact 12 is coupled to first conductive path 16 (i.e., a line side phase conductive path), while second line contact 14 is coupled to second conductive path 18 (i.e., a line side neutral conductive path). Contacts 12, 14 can be in the form of terminal screws, wire leads, or other connections known in the art that can be coupled to a power line. First conductive path 16 and second conductive path 18 form a circuit and in the embodiment shown in FIG. 1A, the first conductive path 16 is arranged to conduct current in the same direction as the second conductive path 18 relative to the sensors 22 and 24. Sensor 20 which can be any one of sensors 22, and 24 may be any suitable sensor known in the art, and may include a single sensor or two or more sensors. In this exemplified embodiment, sensor 20 includes two sensors 22 and 24, wherein one sensor is a high frequency sensor and the other sensor is a low frequency/power line sensor. It should be understood that, although in this embodiment both are depicted (as well as in the embodiments of FIGS. 1B-1H), it is not required to have both a high frequency sensor and a low frequency/power line sensor.

**[0060]** Load side 70 may be separated from line input conductive paths 11 by separable contacts 62, which include separable contacts 64 and 66. Load side 70 includes a first load side conductive path 17, which can be a load side phase line, and a second load side conductive path 19, which can be a load side neutral line. Contact 64 is configured to separate first line side conductive path 16 from first load side conductive path 17 and contact 66 is configured to separate second line side conductive path 18 from second load side conductive path 19.

**[0061]** High frequency sensor 22 may be in the form of any high frequency sensor known in the art. In at least one embodiment, the high frequency sensor 22 may be a transformer having a coil wound around an air core (e.g.—a

Rogowski coil) or a high permeability magnetic core (e.g., an iron powder core where powdered iron is encapsulated in an epoxy substrate). It should be noted that the term “air core” may refer to any core where the core is non-ferrous, e.g., plastic or any suitable material. Low frequency/power line sensor 24 can be in the form of any low frequency sensor known in the art. In at least one embodiment, the low frequency sensor 24 may be a typical current sensor or current transformer.

**[0062]** In addition, in other alternative embodiments, a differential current sensor 26 may be used to detect arc faults to ground. Accordingly, in this view, differential sensor 26 is shown in dashed lines to indicate that it may be optionally used or not used in certain embodiments. This differential sensor 26 may also be employed in the embodiments shown in FIGS. 1B-1H, 3A, 3B, 3C, and 3E. While sensors 20, 22, 24 and 26 are shown in the drawings, the claims are not to be construed as requiring any one of the above listed sensors 20, 22, 24, 26 unless as expressed in writing in those claims.

**[0063]** The high frequency sensor 22, the low frequency sensor 24, and the optional differential sensor 26 are preferably arranged and configured to detect different signals, or conditions, on conductive paths 16 and 18. In at least one embodiment, the low frequency sensor 24 has a high permeability iron powder core. This allows for the core to be manufactured with a relatively small size while avoiding saturation with a wide range of input signals. For example, one type of transformer core (produced by Micrometals, Inc.) is a current transformer core which is close to a standard T50-45 and Al parameter (44.0 nH/(N\*N)), although any other suitable type of transformer can be used as well.

**[0064]** Advantageously, with both a low frequency sensor 24 and a high frequency sensor 22, arc faults can be detected with greater precision and/or reliability. Preferably, each sensor is configured to detect arc faults in the pre-determined frequency range. For example, the low frequency sensor 24 may be configured to detect electrical characteristics of a current path which may be indicative of arc faults at the predetermined frequency range of, preferably a power line frequency or in another embodiment at a higher frequency e.g., 0-2 MHz or 0-4 MHz. The high frequency sensor 22 is preferably configured to detect electrical characteristics of a current path which may be indicative of arc faults at a predetermined frequency range higher than the low frequency sensor, e.g. greater than a predetermined frequency that is in at least one embodiment higher than power line frequency, such as greater than or equal to 1 MHz, alternatively greater than or equal to 2 MHz or greater than or equal to 4 MHz. In certain preferred embodiments, the range for the high frequency sensor 22 may be 1-10, MHz, alternatively, 2-10 MHz, and in other embodiments the range for the high frequency sensor may be 4-10 MHz.

**[0065]** In alternative embodiments, the addition of an optional differential sensor 26 to supplement/complement the high frequency sensor 22 and low frequency sensor 24, creates a system where parallel arc faults to ground can also be detected by measuring the differential current between the phase and neutral conductive paths.

**[0066]** In yet another alternative embodiment, a shunt 25 (see FIGS. 1F and 1H) may be employed. The shunt 25 preferably has a known resistance along its path and can be incorporated into the phase conductive path 16, the neutral